# **Noise-robust synchronized chaotic communications**

# T. L. Carroll US Naval Research Lab Washington, DC 20375 USA

Abstract-- Until now, research on the applications of self-synchronized chaotic circuits to communications has been hindered by the great sensitivity of self synchronized chaotic systems to additive noise. In this paper I demonstrate a self-synchronized chaotic system that synchronizes even in the presence of noise much larger than the signal. This system works because it generates signals with 2 different time scales, allowing noise added to the shorter time scale system to be averaged out by the longer time scale system. I demonstrate a simple communications scheme with this system, and I show that the curve of bit error rate as a function of (energy per bit )/(noise spectral density) is invariant with respect to bit length, allowing this system to operate in arbitrarily low signal-to-noise environments.

#### I. Introduction

Much of the initial research into self-synchronized chaotic systems was motivated by possible applications to communications [1-11], for chaotic circuits are a naturally simple way to produce broad band signals. Self synchronized chaotic systems have suffered from the same problem as transmitted reference spread spectrum systems [12], however; the reference signal is contaminated by noise in the channel. It is probable that self synchronizing methods can never perform as well as stored reference methods (such as CDMA [13]) in the presence of noise, but, as I show in this work, it is possible for self synchronizing chaotic systems to be noise robust according to the definition of Abel et al. [14], which states that a communications system is noise robust if the curve of bit error rate as a function of  $E_b/N_0$  is invariant with respect to bit length. If a communications system is noise robust, operation in arbitrarily low signal-to-noise ratios is possible simply by increasing bit length.

## **II. 2-Frequency Circuit**

It is possible in nature to have chaotic systems where motion occurs on very different time scales; in ferromagnetic resonance experiments in Yttrium Iron Garnet, for example [15-18], the spin magnetic moment of the material responds at frequencies in the range of 10<sup>9</sup> Hz and 10<sup>3</sup> Hz. For a previous paper, a chaotic circuit was designed which also had motion on 2 different time scales [19]. The circuit itself could be divided into a high frequency part and a low frequency part. A signal from the drive circuit was transmitted in order to synchronize a response circuit, but the signal was only coupled into the high frequency part. The low frequency part of the circuit then acted as a filter, and averaged out most of the noise added to the transmitted signal, resulting in small

synchronization errors for the low frequency part even when the signal to noise ratio for the transmitted signal was less than 0 dB.

Synchronization alone is not enough, of course; it must also be possible to transmit an information signal. In this paper, the 2-frequency system is used to simulate a simple phase modulation communications scheme, and the performance of the communications scheme is measured when noise is added to the transmitted signal.

The transmitter circuit is described by

$$\frac{d\theta}{dt} = \omega 
\frac{dx_1}{dt} = -\alpha_1 (0.02x_1 + 0.5x_2 + x_3 + 0.5|x_4| - k(s_1 \sin(\theta) - \beta x_1)) 
\frac{dx_2}{dt} = -\alpha_1 (-x_1 + 0.02x_2 + x_6) 
\frac{dx_3}{dt} = -\alpha_1 (-g(x_1) + x_3) 
\frac{dx_4}{dt} = -\alpha_2 (x_1 + 0.05x_4 + 0.5x_5 + x_6) 
\frac{dx_5}{dt} = -\alpha_2 (-x_4 + 0.11x_5) 
\frac{dx_6}{dt} = -\alpha_3 (-g(x_4) + x_6) 
g(x) = \begin{cases} 0 & x < 3 \\ 15(x - 3) & x \ge 3 \end{cases}$$
(1)

where  $\alpha_I$  and  $\alpha_2$  may be varied to alter the relative time scales of the two parts of the circuit. The signals  $x_I$  through  $x_3$  form the low frequency part of the circuit, while  $x_4$  through  $x_6$  form the high frequency part. The signal  $\theta$  is the phase control signal, used to modulate the phase of the low frequency part of the oscillator in order to communicate. The frequency  $\omega$  is set equal to the peak frequency of the low frequency part of the oscillator, and the signal  $\theta$  is coupled into the low frequency part in order to phase

synchronize the oscillator [20]. The information signal,  $s_I$ , is set equal to  $\pm 1$ , while the coupling constant k = 0.2, and  $\beta = 0.37$ .

Figure 1(a) shows the power spectrum S of the  $x_1$  signal measured from eq. (1) while Fig. 1(b) shows the power spectrum S of the  $x_4$  signal measured from eq. (1) when  $\alpha_1 = 0.2$  and  $\alpha_2 = 10.0$ , so that the time scales are separated by a factor of 50. The higher frequency peak in the power spectrum, most prominent in Fig. 1(b), is at 1.1 Hz. The lower frequency peak in the power spectrum, largest in Fig. 1(a), is at 0.022 Hz. Choosing different values for  $\alpha_1$  and  $\alpha_2$  changed the ratio of the two frequencies.

The signal that was transmitted from drive to response,  $x_t$ , was a linear combination of signals from the drive system. The response circuit was described by

$$x_{t} = \sum_{i=1}^{6} k_{i} x_{i}^{d} + \eta \qquad x_{r} = \sum_{i=1}^{6} k_{i} x_{i}^{r}$$

$$\frac{dx^{r}_{1}}{dt} = -\frac{1}{RC_{1}} \left( \gamma_{1} x^{r}_{1} + 0.5 x^{r}_{2} + x^{r}_{3} + 0.5 \middle| x^{r}_{4} \middle| \right)$$

$$\frac{dx^{r}_{2}}{dt} = -\frac{1}{RC_{1}} \left( -x^{r}_{1} + \gamma_{2} x^{r}_{2} + x^{r}_{6} \right)$$

$$\frac{dx^{r}_{3}}{dt} = -\frac{1}{RC_{1}} \left( -g(x^{r}_{1}) + x^{r}_{3} \right)$$

$$\frac{dx^{r}_{4}}{dt} = -\frac{1}{RC_{2}} \left( x^{r}_{1} + 0.05 x^{r}_{4} + 0.5 x^{r}_{5} + x^{r}_{6} + b_{4}(x_{t} - x_{r}) \right)$$

$$\frac{dx^{r}_{5}}{dt} = -\frac{1}{RC_{2}} \left( -x^{r}_{4} + 0.11 x^{r}_{5} + b_{5}(x_{t} - x_{r}) \right)$$

$$\frac{dx^{r}_{6}}{dt} = -\frac{1}{RC_{2}} \left( -g(x^{r}_{4}) + x^{r}_{6} + b_{6}(x_{t} - x_{r}) \right)$$

where the superscript d refers to the drive circuit and r refers to the response circuit and  $\eta$  is a Gaussian noise signal filtered to match the bandwidth of the response system (the

determination of the bandwidth is described below). Note that the error signal  $x_t$  -  $x_r$  is fed back only into the high frequency part of the circuit,  $x_4$  to  $x_6$ .

The parameters  $k_i$  and  $b_i$  are set to minimize the largest Lyapunov exponent for the response circuit corresponding to eq. (2) [21, 22]. The  $k_i$ 's and  $b_i$ 's are varied by a linear optimization routine in order to minimize the largest Lyapunov exponent for the response circuit. For the parameters listed in Table 1, the largest Lyapunov exponent for the response circuit was -0.22 s<sup>-1</sup> when  $\alpha_i$  was 0.2 and  $\alpha_2$  was 10.0. Varying  $\alpha_i$  and  $\alpha_2$  changed the stability of the response system, but the largest Lyapunov exponent remained negative for a large range of  $\alpha$ 's, so the same  $k_i$ 's and  $b_i$ 's were used for all simulations.

### **III Communication**

The systems of eqs. (1-2) were simulated in order to test the communications performance of this type of circuit. The information signal  $s_I$  in eq. (1) was set to  $\pm 1$  to simulate a binary signal. The value of  $s_I$  determined the phase of the low frequency part of eq. (1). The receiver of eq. (2) was used to measure the phase of the low frequency part of eq. (1) in order to determine the value of  $s_I$ . The phase detector part of the receiver was

$$\frac{d\theta^r}{dt} = \omega$$

$$\frac{du}{dt} = \frac{dx_4^r}{dt} - \frac{\alpha_1}{100.0}u$$

$$v = \operatorname{sgn}[\sin(\theta^r)]u$$

$$\frac{dw}{dt} = \frac{\alpha_1}{10.0}(v - 0.1w)$$
(3).

The frequency  $\omega$ , the frequency of the local reference oscillator in the response system, was the same frequency as in eq. (1). The signal u was a high-pass filtered version of  $x_4^r$ ,

high-pass filtered because the absolute value function in eq. (2) produced a DC offset in  $x'_4$  when the noise signal was large. The "sgn" function is the signum function (+1 for the argument > 0, -1 for the argument < 0). The variable w in eq. (3) is set to zero at the start of each bit interval, and w is measured at the end of each bit interval to determine the value of the received bit.

The necessary bandwidth for the chaotic signal is found by measuring the bit error rate. A low pass filtered noise signal is added to a low pass filtered version of the signal  $x_t$  and the resulting bit error rate is measured at the receiver as the filter breakpoint is lowered. At some given breakpoint, the bit error rate is seen to increase, so the filter breakpoint is set larger than this value. For the system in this paper, the minimum filter breakpoint was 7.5 Hz.

Figure 2 shows the probability of bit error  $P_b$  for the system of eqs. (1-3). The dark circles show  $P_b$  for a bit length of L = 653.9 s, in which case  $\alpha_I$  was set to 0.2 and  $\alpha_2$  was set to 10.0. The open circles show  $P_b$  for a bit length of L = 1307.84 s (twice as long), with  $\alpha_I = 0.1$  and  $\alpha_2 = 10.0$ . The energy per bit/(noise power spectral density)  $(E_b/N_0)$  is calculated for a 2-sided noise power spectrum. The two sets of data lie along the same curve, demonstrating that the curve of  $P_b$  vs.  $E_b/N_0$  does not depend on bit length, a property not yet seen in other transmitted reference chaotic communication systems. The solid line in Fig. 2 shows the probability of bit error for binary phase shift keying (BPSK) [23] for comparison.

The noise robustness of this system may be further explored by changing the bit length L and finding the probability of bit error at a constant value of  $E_b/N_0$ . In Figure 3,  $E_b/N_0$  is held constant at 14.3 dB while the bit length L is varied by a factor of 32, from

653.9 s to 20,924.8 s. The slow time constant  $\alpha_I$  is varied at the same time the bit length is varied, so  $\alpha_I$  varies from 0.2 to 0.2/32 = 0.00625, while  $\alpha_2$  is held constant at 10.0. The upper scale in Fig. 3 shows the signal to noise ratio in decibels. The probability of bit error is seen to be roughly constant when the bit length L varies by a factor of 32, demonstrating that this self-synchronizing chaotic system is noise robust for added Gaussian noise. In addition, the performance of this communications system does not degrade when the signal to noise ratio is below 0 dB.

In order to demonstrate that the transmitted signal is truly being buried in the noise, Figure 4(a) shows the power spectrum S of the transmitted signal  $x_t$  when  $\alpha_t = 0.00625$  and  $\alpha_2 = 10.0$ . Fig. 4(b) shows the same signal with added Gaussian noise so that the S/N is approximately -43 dB (corresponding to the longest bit length used in Fig. 3). The added noise covers even the peaks in the power spectrum of  $x_t$ . The high frequency peak is about 20 dB below the noise level, while the low frequency peak is at approximately the same level as the noise.

#### **IV Conclusions**

Transmitted reference communications systems should not be noise robust, since noise is added to the reference signal, and studies for chaotic transmitted reference signals confirm this supposition [14]. Self-synchronizing chaotic systems are not transmitted reference systems such as DCSK [24, 25], but are nonlinear filters. In this way they are more general versions of periodic methods such as BPSK, which uses linear filters to isolate the signal from noise. Self-synchronizing chaotic systems are not as efficient as purely periodic systems because the nonlinear filter (the chaotic response system) has a larger bandwidth, so less noise is excluded.

Phase modulation was used in this paper as a simple example to demonstrate that communication is possible with 2-frequency synchronized chaotic systems, but it is probably not the most efficient way to use these systems. A 2-frequency system might be more useful as a filter for communication involving symbolic dynamics, in which chaotic trajectories form the communications symbols [26].

### References

- [1] L. M. Pecora and T. L. Carroll, "Synchronization in Chaotic Systems," *Physical Review Letters*, vol. 64, Feb., pp. 821-824, 1990.
- [2] T. L. Carroll and L. M. Pecora, "Synchronizing Chaotic Circuits," *IEEE Transactions on Circuits and Systems*, vol. 38, April, pp. 453-456, 1991.
- [3] K. M. Cuomo, A. V. Oppenheim, and S. H. Strogatz, "Synchronization of Lorenz-Based Chaotic Circuits with Applications to Communications," *IEEE Transactions on Circuits and Systems*, vol. 40, Oct., pp. 626-633, 1993.
- [4] T. L. Carroll, "Communicating using Filtered Synchronized Chaotic Signals," *IEEE Transactions on Circuits and Systems*, vol. 42, Feb., pp. 105-110, 1995.
- [5] T. L. Carroll, J. F. Heagy, and L. M. Pecora, "Transforming signals with chaotic synchronization," *Physical Review E*, vol. 54, Nov., pp. 4676-4680, 1996.
- [6] L. Kocarev, K. S. Halle, K. Eckert, L. O. Chua, and U. Parlitz, "Experimental Demonstration of Secure Communications via Chaotic Synchronization," *International Journal of Bifurcations and Chaos in Applied Science and Technology*, vol. 2, Sept., pp. 709-713, 1992.

- [7] G. Kolumban, M. P. Kennedy, and L. O. Chua, "The Role of Synchronization in Digital Communications Using Chaos-Part I: Fundamentals of Digital Communications," *IEEE Transactions on Circuits and Systems-Part I:*Fundamental Theory and Applications, vol. 44, 10, pp. 927-935, 1997.
- [8] K. Murali and M. Lakshmanan, "Transmission of signals by synchronization in a chaotic Van der Pol-Duffing oscillator," *Physical Review E*, vol. 48, Sept., pp. 1624-1626, 1993.
- [9] U. Parlitz, L. Kocarev, T. Stojanovski, and H. Prekel, "Encoding messages using chaotic synchronization," *Physical Review E*, vol. 53, May, pp. 4351-4361, 1996.
- [10] E. Rosa, S. Hayes, and C. Grebogi, "Noise Filtering in Communication with Chaos," *Physical Review Letters*, vol. 78, no. 7, pp. 1247-1250, 1997.
- [11] N. F. Rulkov and L. Tsimring, "Communication with Chaos over Band-Limited Channels," *International Journal of Circuit Theory and Applications*, vol. 27, no. 6, pp. 555-567, 1999.
- [12] R. C. Dixon, *Spread Spectrum Systems with Commercial Applications*. New York: Wiley, 1994.
- [13] A. J. Viterbi, *CDMA: Principles of Spread Spectrum Communication*. Reading, MA: Addison-Wesley, 1995.
- [14] A. Abel, W. Schwartz, and M. Goetz, "Noise Performance of Chaotic Communication Systems," *IEEE Transactions on Circuits and Systems*, vol. 47, no. 12, pp. 1726-1732, 2000.
- [15] G. Gibson and C. Jeffries, *Physical Review A*, vol. 29, no. 811, 1984.

- [16] S. M. Rezende, O. F. d. A. Bonfim, and F. M. d. Aguiar, *Physical Review B*, vol. 33, no. 5153, 1986.
- [17] X. Y. Zhang and H. Suhl, *Physical Review A*, vol. 32, no. 2530, 1985.
- [18] T. L. Carroll, L. M. Pecora, and F. J. Rachford, "Chaos and Chaotic Transients in an Yttrium Iron Garnet Sphere," *Physical Review A*, vol. 40, no. 1, pp. 377-386, 1989.
- [19] T. L. Carroll, "Noise resistant chaotic synchronization," *submitted to Physical Review E*, 2000.
- [20] A. S. Pikovsky, M. G. Rosenblum, G. V. Osipov, and J. Kurths, "Phase Synchronization of Chaotic Oscillators by External Driving," *Physica D*, vol. 104, no. 3-4, pp. 219-238, 1997.
- [21] J. H. Peng, E. J. Ding, M. Ding, and W. Yang, "Synchronizing Hyperchaos with a Scalar Transmitted Signal," *Physical Review Letters*, vol. 76, no. Feb, pp. 904-907, 1996.
- [22] G. A. Johnson, D. J. Mar, T. L. Carroll, and L. M. Pecora, "Synchronization and imposed bifurcations in the presence of large parameter mismatch," *Physical Review Letters*, vol. 80, no. 18, pp. 3956-3959, 1998.
- [23] B. Sklar, Digital Communications, Fundamentals and Applications.Englewood Cliffs, NJ: Prentice Hall, 1988.
- [24] M. P. Kennedy, G. Kolumban, and G. Kis, "Chaotic Modulation for Robust Digital Communications over Multipath Channels," *International Journal of Bifurcations and Chaos in Applied Science and Engineering*, vol. 10, no. 4, pp. 695-718, 2000.

- [25] G. Kolumban, "Basis function description of chaotic modulation schemes," proceedings of Nonlinear Dynamics of Electronic Systems, Catania, 2000, pp. 165-169.
- [26] S. Hayes, C. Grebogi, E. Ott, and A. Mark, "Experimental Control of Chaos for Communication," *Physical Review Letters*, vol. 73, Sept., pp. 1781-1784, 1994.

i	$k_i$	$b_{i}$
1	5.34	0
2	-2.58	0
3	-3.10	0
4	1.60	-0.53
5	-0.89	0.34
6	-1.61	-0.23

Table 1. Values of  $k_i$  and  $b_i$  parameters.

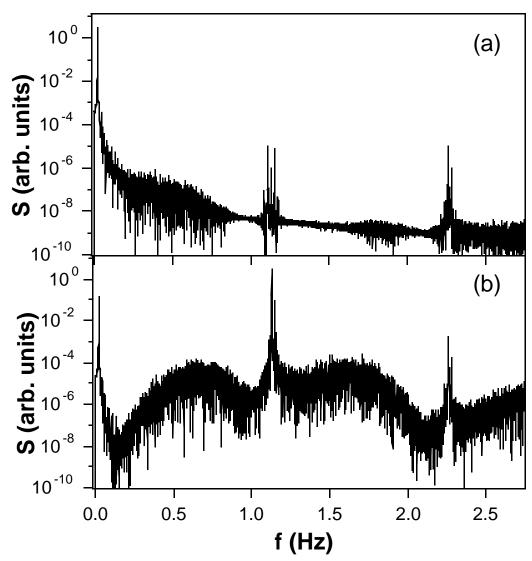


Figure 1. Power spectra S for the system of eq. (1) when  $\alpha_1 = 0.2$  and  $\alpha_2 = 10.0$ . (a) is the power spectrum of  $x_1$ , while (b) is the power spectrum of  $x_4$ .

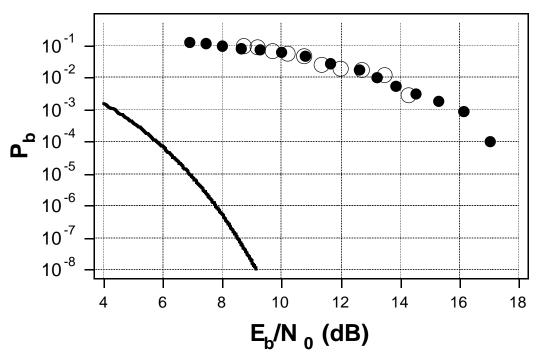


Figure 2. Probability of bit error  $P_b$  as a function of (energy per bit)/(2 sided noise power spectral density) ( $E_b/N_0$ ) for the communications system described by eqs. (1-3). The filled in circles are for a bit length of L=653.9 s, while the open circles are for L twice as long. The solid line is for binary phase shift keying (BPSK).

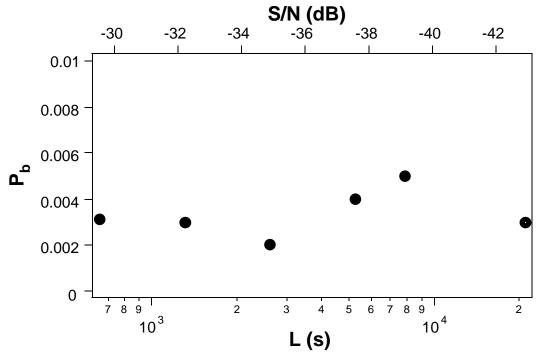


Figure 3. Probability of bit error  $P_b$  for different bit lengths L at a constant  $E_b/N_0$  of 14.3 dB. L varies by a factor of 32. The top axis is the corresponding signal to noise ratio.

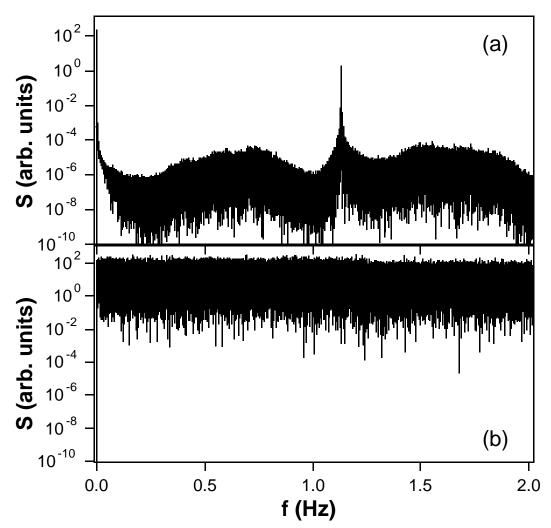


Figure 4. (a) is the power spectrum S of the transmitted signal  $x_t$  when the time factors are  $\alpha_t = 0.00625$  and  $\alpha_2 = 10.0$ . (b) is  $x_t$  with added noise corresponding to the largest value of L in Fig. (3), so that the signal to noise ratio is approximately -43 dB.